AMENDMENT(S) TO THE SPECIFICATION

Please replace the paragraph beginning at page 8, line 14, with the following rewritten paragraph:

In addition to improving strength at high temperatures by dissolving into the matrix in the form of the γ phase in the presence of W and Ta, Mo also improves strength at high temperatures due to precipitation hardening. Furthermore, Mo also improves the aftermentioned lattice misfit and dislocation ~~networks~~ space of the alloy which relate characteristics of this alloy.

Please replace the paragraph beginning at page 11, line 6, with the following rewritten paragraph:

Particularly in the present invention, by adjusting the composite ratios of Al, Ta, Mo, W, Hf, Cr, Co and Ni to the optimum ratios, together ~~with improving strength at high temperatures~~ by setting the aftermentioned lattice misfit and dislocation ~~networks~~ space of the alloy which are calculated from the lattice constant of the γ phase and the lattice constant of the γ' phase within their optimum ranges, strength at high temperatures is improved, and precipitation of the TCP phase can be inhibited by adding Ru. Furthermore, by adjusting the composite ratios of Al, Cr, Ta and Mo to the aforementioned ratios, the production cost for the alloy can be decreased. In addition, relative strength of the alloy can be increased and the lattice misfit and dislocation ~~networks~~ space of the alloy can be adjusted to the optimum value.

Please replace the paragraph beginning at page 12, line 17, with the following rewritten paragraph:

Ti can be further included in the above Ni-based super crystal super alloy. The composite ratio of ~~Ta~~ Ti is preferably within the range of 0 wt% or more to 2.0 wt% or less. If the composite ratio of Ti exceeds 2.0 wt%, the harmful phase precipitates and the strength at high temperatures cannot be maintained, thereby making this undesirable.

Please replace Table 3 at the beginning at page 16 with the following rewritten Table 3

Table 3

Sample (alloy name)	Creep test conditions/rupture life (h)		Lattice Misfit
	1273K (1000°C) 245 Mpa	1373K (1100°C) 137MPa	
Reference Example 1	209.35	105.67	-0.39
Reference Example 2	283.20	158.75	-0.40
Reference Example 3	219.37	135.85	-0.56
Reference Example 4	274.38	153.15	-0.58
Reference Example 5	328.00	487.75	-0.58
Reference Example 6		203.15	-0.41
Embodiment 1	509.95 ~~5.09.95~~	326.50 ~~32.6.50~~	-0.60
Embodiment 2	420.60	753.95	-0.42
Embodiment 3		1062.50	-0.62
Embodiment 4		966.00	-0.44
Embodiment 5		1256.00	-0.48
Embodiment 6		400.00	-0.45
Embodiment 7		1254.00	-0.60
Embodiment 8		682.00	-0.63
Embodiment 9		550.00	-0.42
Embodiment 10		658.50	-0.45
Embodiment 11		622.00	-0.48
Embodiment 12		683.50	-0.51
Embodiment 13	412.7	766.35	-0.62
Embodiment 14		1524.00	-0.45

Please replace Table 5 at the beginning at page 18 with the following rewritten Table 5:

Table 5

Sample (alloy name)	Withstand temperature (°C)
Reference Example 1	1315K (1042°C)
Reference Example 2	1325K (1052°C)
Reference Example 3	1321K (1048°C)
Reference Example 4	1324K (1051°C)
Reference Example 5	1354K (1081°C)
Reference Example 6	1332K (1059°C)
Embodiment 1	1344K (1071°C)
Embodiment 2	1366K (1093°C)
Embodiment 3	1375K ~~(1102C)~~ (1102°C)
Embodiment 4	1372K (1099°C)
Embodiment 5	1379K (1106°C)
Embodiment 6	1379K (1106°C)
Embodiment 7	~~1379K (1106°C)~~ 1349K (1076°C)
Embodiment 8	1363K (1090°C)
Embodiment 9	1358K (1085°C)
Embodiment 10	1362K (1089°C)
Embodiment 11	1361K (1088°C)
Embodiment 12	1363K (1090°C)
Embodiment 13	1366K (1093°C)
Embodiment 14	1384K (1111°C)
Comparative Example 1 (CMSX-2)	1289K (1016°C)
Comparative Example 2 (CMSX-4)	1306K (1033°C)
Comparative Example 3 (Rene'N6)	1320K (1047°C)
Comparative Example 4 (CMSX-10K)	1345K (1072°C)
Comparative Example 5 (3B)	1353K (1080°C)